

A Fast, Self-stabilizing, Boost DC-DC Converter - Sliding-mode Vs Hysteretic Controls

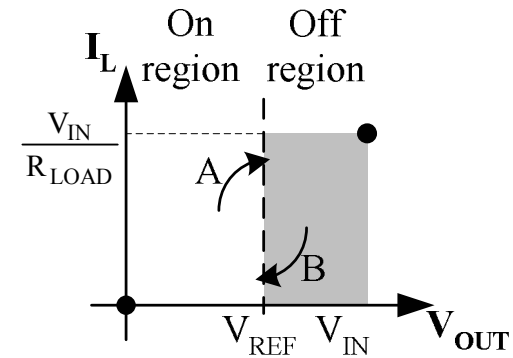
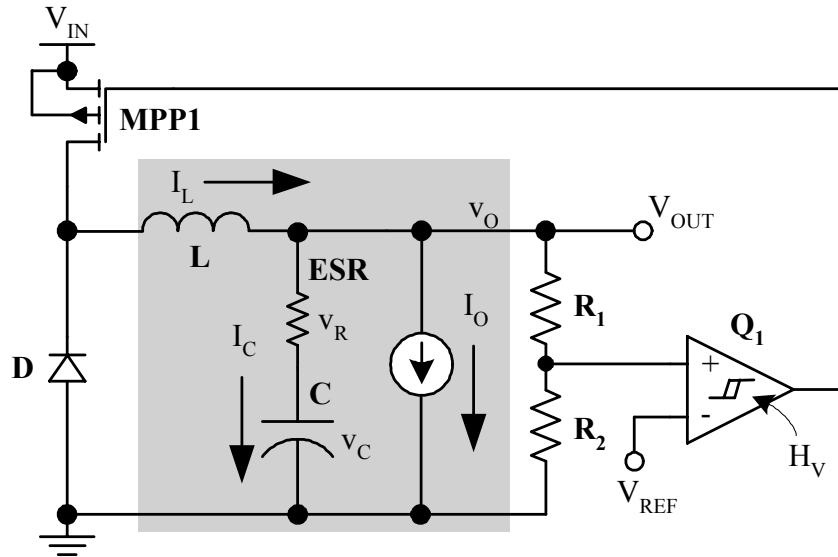
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Motivation

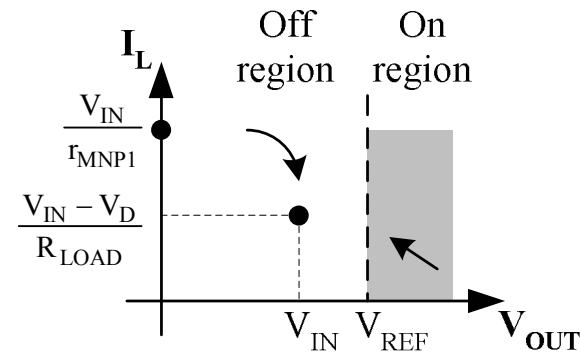
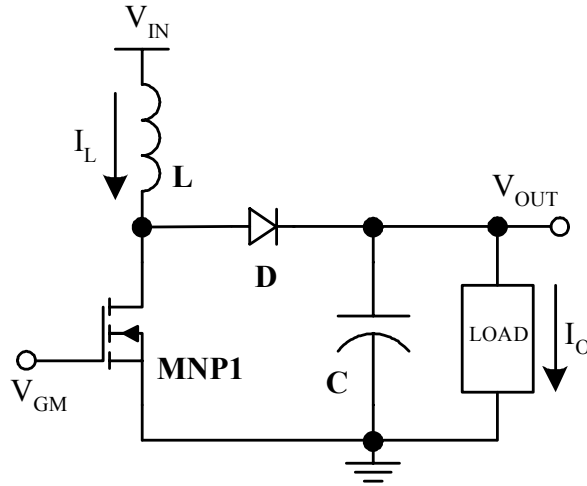
- Significant dependence of converter frequency response on passive components
- Tolerances in capacitor ESR, ESL values
- Variations in inductor, capacitor values per design
- IC solution for frequency compensation required because
 - Reduction in design time
 - Reduction in part count
 - Reduction in board size, cost
 - Ease of design
- *Need to have IC solution that will give frequency compensation independent of external components*
- **Hysteretic control provides a way !**

Hysteretic Buck Converter



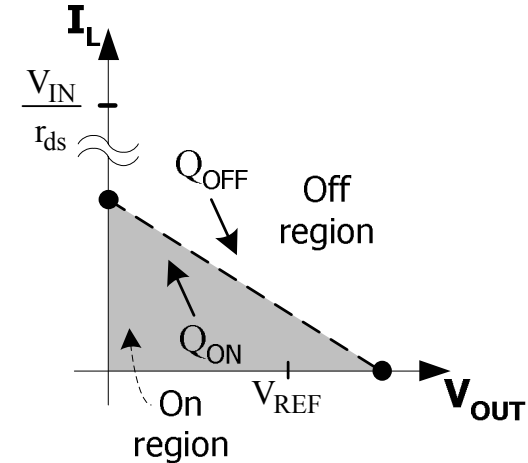
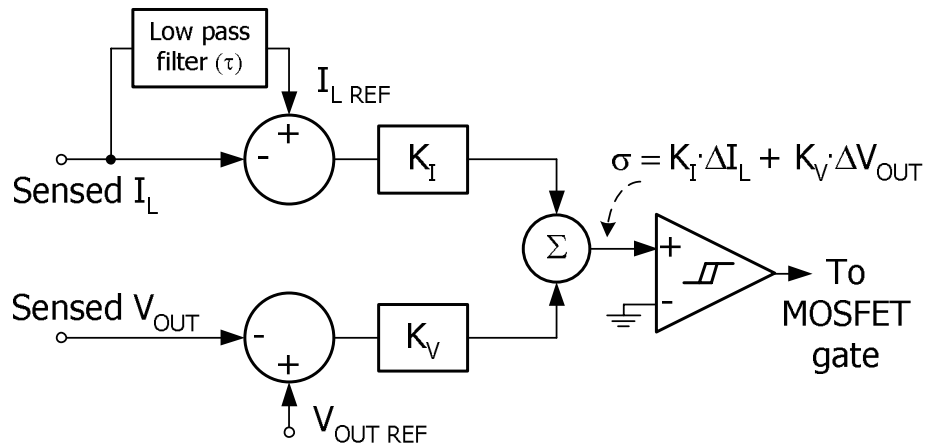
- Hysteretic control regulates **output voltage ripple v_o**
- With switch MPP1 held on: $V_{OUT} = V_{IN}$
- With switch MPP1 held off: $V_{OUT} = 0$
- V_{REF} is between "ON" and "OFF" regions, forming "**switching surface**"
- *System state moves towards switching surface from either side*

Issues with Hysteretic Control in Boost Converters



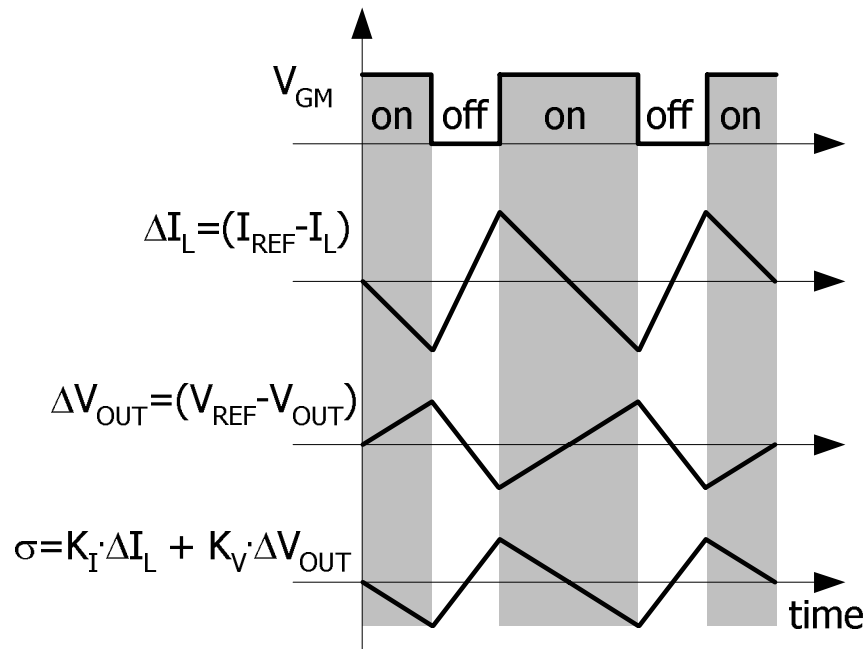
- With switch MNP1 held on: $V_{OUT} = 0$
- With switch MNP1 held off: $V_{OUT} = V_{IN}$
- V_{REF} is **not** between "ON" and "OFF" regions
- *System state does not move towards V_{REF} from either side*

Solution 1: Sliding-mode Control



- Variable regulated is σ , which is a combination of I_L and V_{OUT}
- Variable $\sigma = K_I \cdot (I_{\text{REF}} - I_L) + K_V \cdot (V_{\text{REF}} - V_{\text{OUT}})$
- Control regulates $\sigma = 0$ using hysteretic controller
- At DC, $I_{\text{REF}} = I_L$, hence if $\sigma = 0$, then $V_{\text{REF}} = V_{\text{OUT}}$

Sliding-mode Control (contd.)



For stability:

$$\left(\frac{d\sigma}{dt} \right)_{\text{ON}} < 0$$

$$\left(\frac{d\sigma}{dt} \right)_{\text{OFF}} > 0$$

Hence,

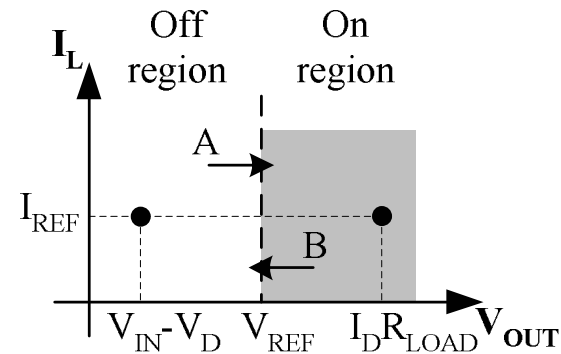
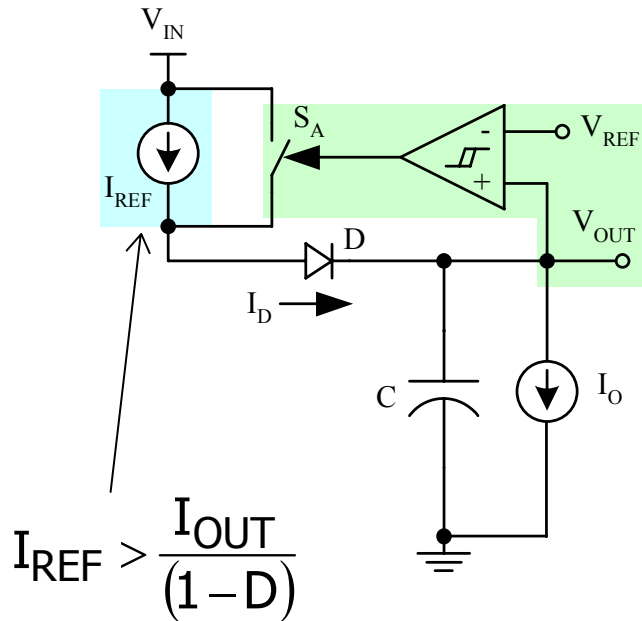
$$|K_I \Delta I_L| > |K_V \Delta V_{\text{OUT}}|$$

Hence, for boost converters: $\frac{K_I}{K_V} > \frac{L}{R_{\text{LOAD}} C (1-D)}$

X For large L and small C, $K_I \gg K_V$, giving slower, multiple cycle transient

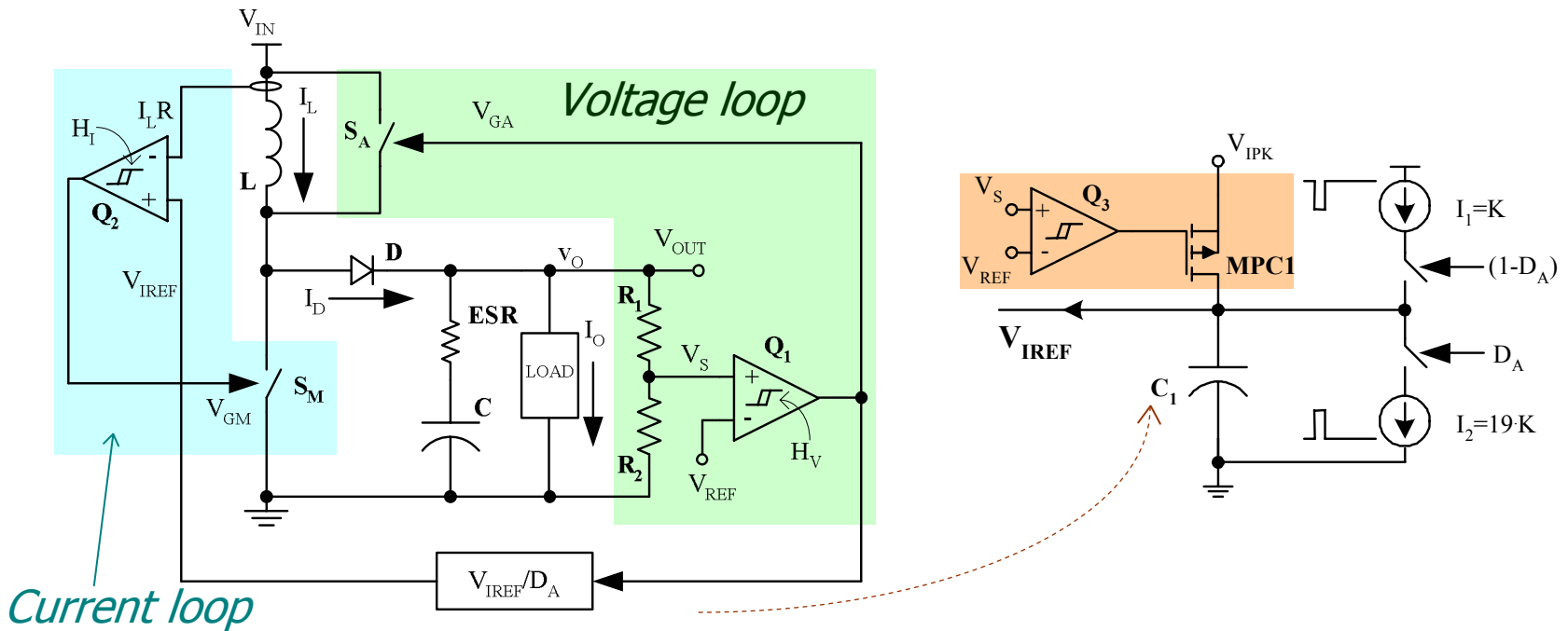
X Also, τ of low pass filter needs to be large slowing transient response

Solution 2: Novel Hysteretic Control



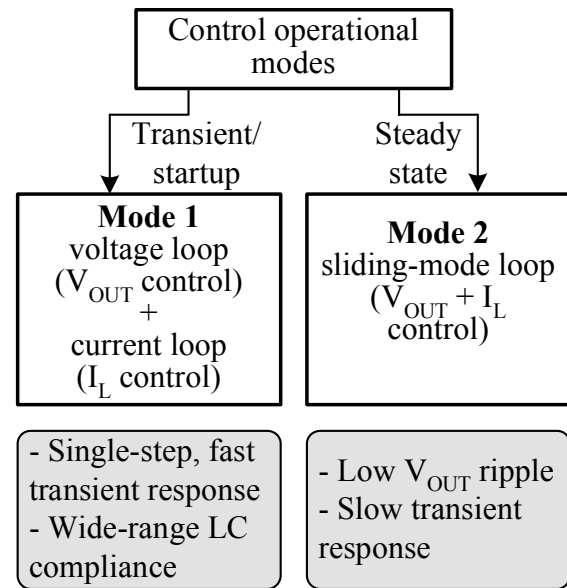
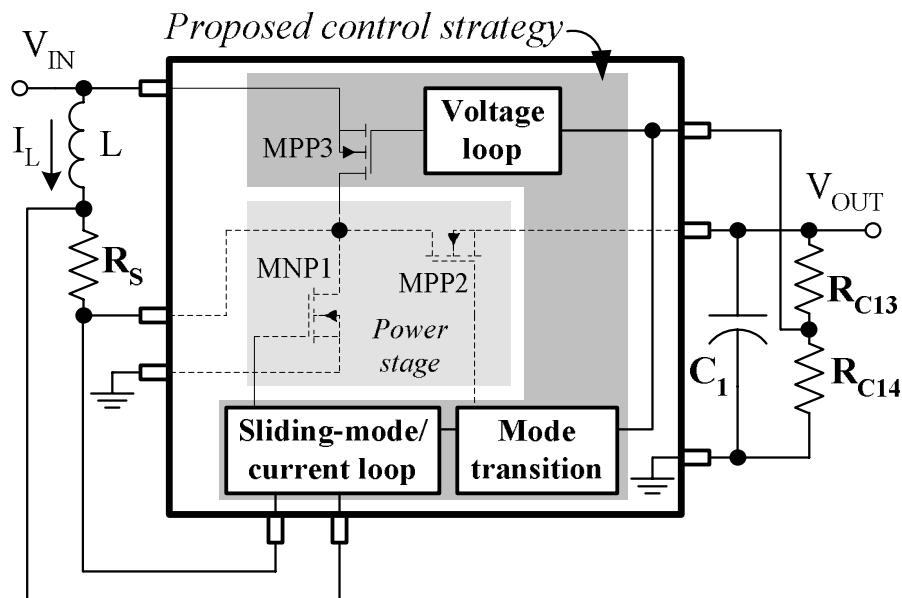
- With switch S_A held on: $V_{OUT} = 0$
- With switch S_A held off: $V_{OUT} = I_D R_{LOAD} > V_{REF}$
- V_{REF} is between "ON" and "OFF" regions
- *System state moves towards V_{REF} from either side*

Novel Hysteretic Control (contd.)



- ✓ Fast, single-step (slew-limited) transient response for all filter LC values
- ✗ Somewhat large steady-state output voltage ripple
- ✗ Lower high-load efficiency because of higher inductor current

Combined Control Strategy

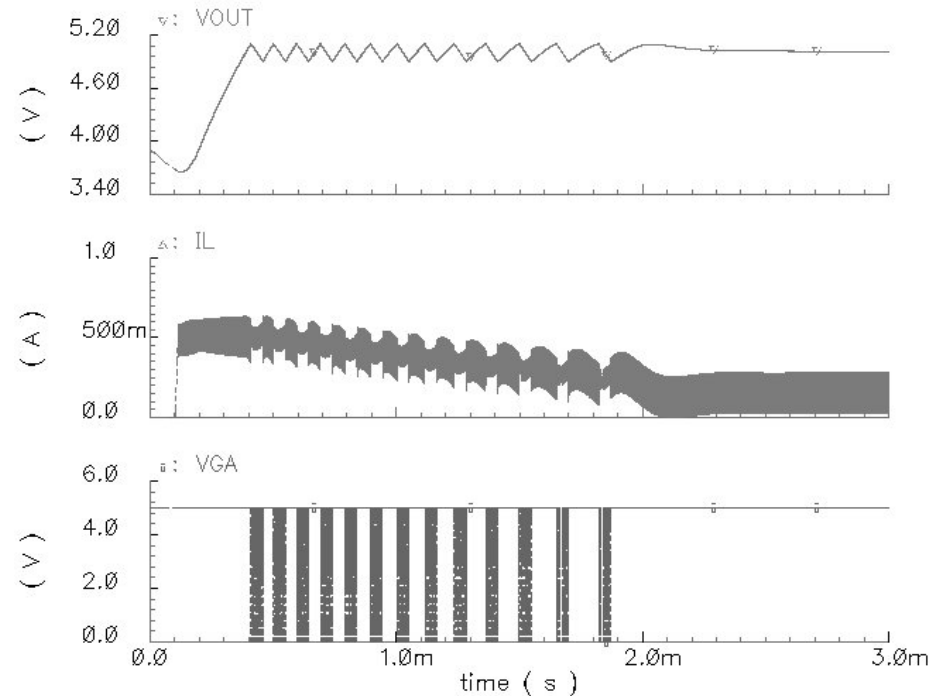
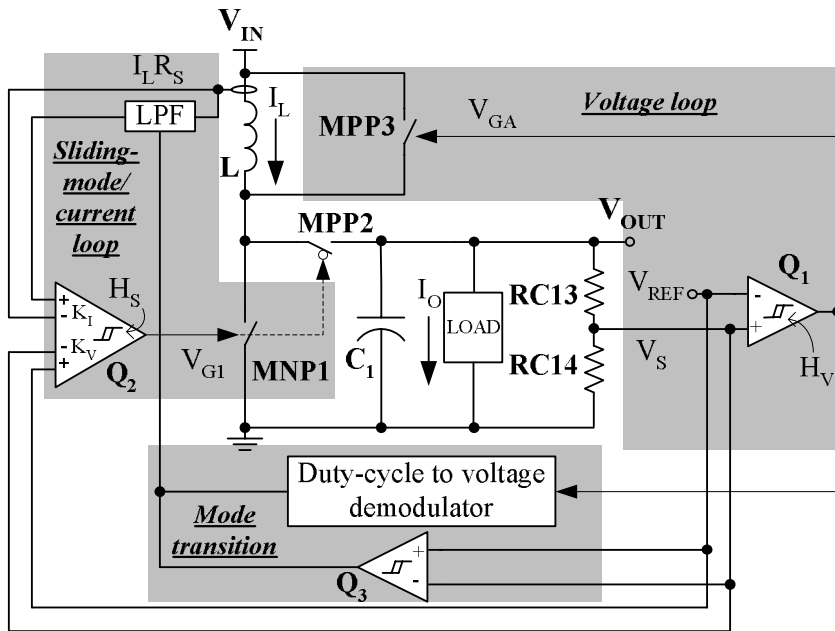


Combination of two previous strategies in multi-mode system

Mode 1 (Hysteretic control): Operated during transient for fast response

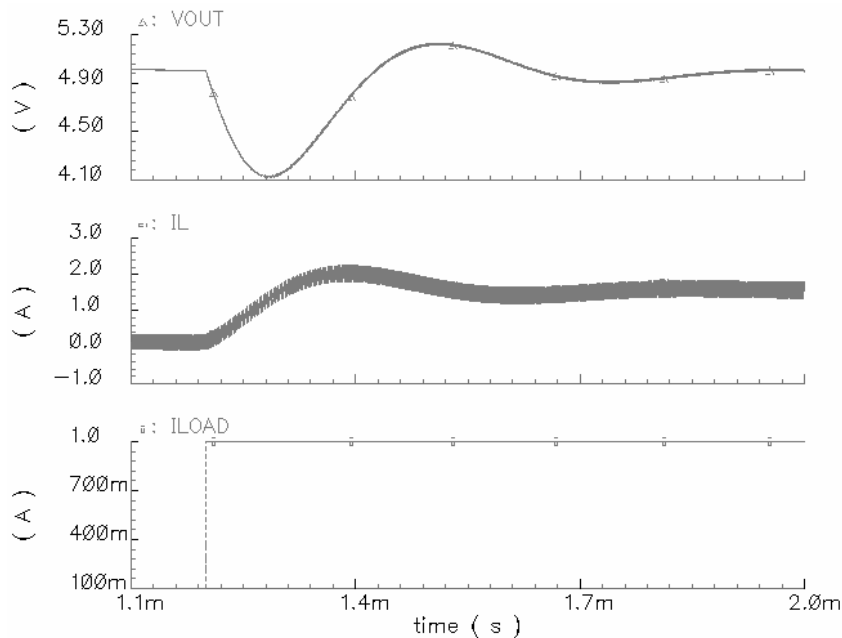
Mode 2 (sliding-mode control): Operated during steady-state for low ripple

Combined Control Strategy (contd.)

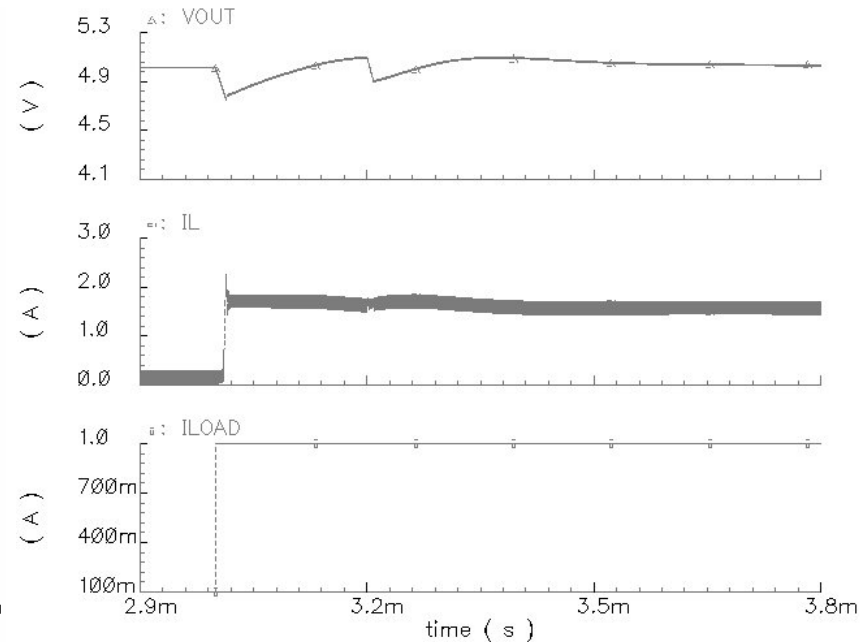


- Start-up under hysteretic mode with higher voltage ripple; inductor current higher than that at steady-state value with switch MPP3 switching
- Inductor current decreased by duty-cycle to voltage demodulator until steady state; switch MPP3 then stops switching

Comparison of Load Transient Response



Sliding-mode control



Proposed control

- Load step response: I_{LOAD} from 0.1 to 1 A, $L = 5 \mu\text{H}$, $C = 47 \mu\text{F}$
- Proposed technique gives a ΔV_{OUT} improvement of more than 650 mV, which is $\sim 13\%$ of V_{OUT}

Conclusions

- A new multi-mode control strategy was introduced in boost DC-DC converters, combining speed advantages of hysteretic control and low steady-state ripple of sliding-mode control
- This strategy enables a de-coupling between the conflicting requirements of greater relative stability and fast transient response
- Wide variations in LC filter parameters can be accommodated without the use of any external frequency compensation circuit
- Fast, single-step (slew-limited) load transient response obtained in the proposed strategy for a wide range of LC filter parameters as against a compensation bandwidth limited response in conventional control
- An optimal boost DC-DC converter control strategy was introduced as most suitable for integration enabling a simple, user-friendly, and effective solution